

PACKING

CHESTERTON[®] PACKING STANDARDIZATION
GUIDELINES FOR THE PULP AND
PAPER INDUSTRY



Chesterton's packing and gaskets are specifically designed to simplify installation, improve reliability and extend performance of your fluid handling equipment.

This guide provides standardization guidelines for the Pulp and Paper Industry.

THE RELIABILITY-CENTERED ROTATING EQUIPMENT PROGRAM

Chesterton offers extensive experience increasing the reliability and energy efficiency of mission-critical rotating equipment throughout the world's largest pulp and paper plants. With an in-depth understanding of paper mill equipment tough applications, we deliver long-lasting solutions for optimal performance and profitability.

Turn to Chesterton for:

- **Maximum Pump Performance:** A complete portfolio of innovative mechanical seals and pump packing, high performance lubricants, and industrial coatings—plus the invaluable advice of our on-call regional experts.
- **Asset Repairs/Protection:** High performance industrial lubricants and coatings that protect new equipment against the forces of corrosion and abrasions and often significantly extend the life of older equipment.
- **Energy/Water Reduction:** Water and energy reduction programs that can result in dramatic savings and high sustainability ratings for your organization.

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DUALPAC® 2211 PACKING

Severe slurry service packing

APPLICATION PARAMETERS

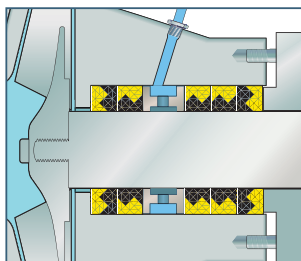
Temperature: 260°C (500°F)

Chemical: pH 3 – 11

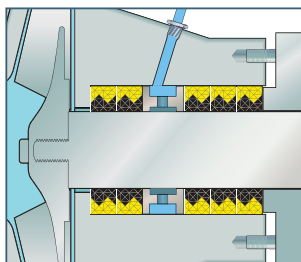
Speed: 10 m/s (2000 fpm)

EQUIPMENT TYPE AND SERVICE

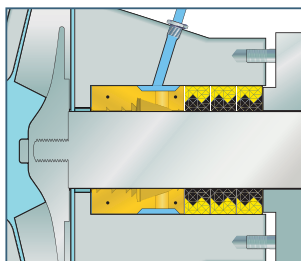
Slurry agitators, pumps, mixers,
and tailing water.



Solid resistance and
anti-extrusion



All rings oriented
for sealing



Chesterton® DualPac®
SuperSet™ Packing Set



DUALPAC® 2212 PACKING

Severe slurry service packing

APPLICATION PARAMETERS

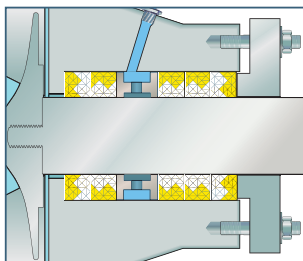
Temperature: 260°C (500°F)

Chemical: pH 3 – 11

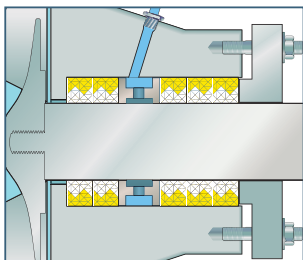
Speed: 10 m/s (2000 fpm)

EQUIPMENT TYPE AND SERVICE

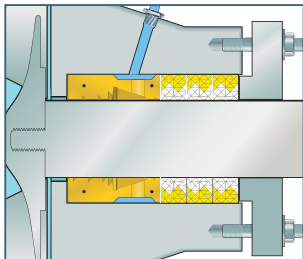
Slurry agitators, pumps, mixers, and tailing water. Can be used where coloration of the product is an issue (non-staining).



Solid resistance and anti-extrusion



All rings oriented for sealing



Chesterton® DualPac®
SuperSet™ Packing Set

 DualPac®
Technology



1830 PACKING

Graphite PTFE packing

APPLICATION PARAMETERS

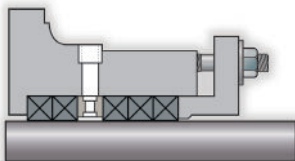
Temperature: 260°C (500°F)

Chemical: pH 0 – 14, except strong oxidizers in 0 – 2 pH range

Speed: 18 m/s (3600 fpm)

EQUIPMENT TYPE AND SERVICE

Mild chemicals (pH 5 – 9), strong acids (pH 1 – 4), centrifugals (also mech. seals), hydropulpers, hydrofiners, refiners, stock chests, cold water shafts, high density stock pumps, and vacuum pumps.



1830 SSP PACKING

Slurry packing

APPLICATION PARAMETERS

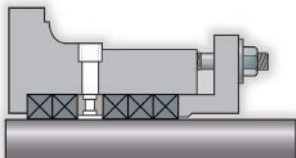
Temperature: Max. temp. 260°C (500°F)

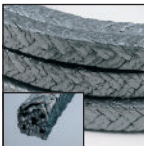
Chemical: pH range 0 – 14, except strong oxidizers in the 0 – 2 pH range

Speed: 18 m/s (3600 fpm)

EQUIPMENT TYPE AND SERVICE

Strong acids (pH 1-4), valves and reciprocating, centrifugals, stock pumps, jordans, claffins, hydropulpers, hydrofiners, refiners, stock chests, white water pumps, white liquor pumps, black liquor pumps, green liquor pumps, and evaporators.





1400R PACKING

Carbon-reinforced graphite tape

APPLICATION PARAMETERS

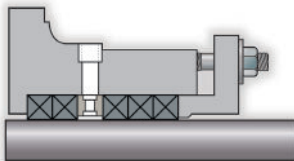
Temperature: 650°C (1200°F) steam;
455°C (850°F) oxidizing atmosphere

Chemical: pH 0 – 14 except oleum,
fuming nitric acid, and aqua regia

Speed: 20 m/s (4000 fpm)

EQUIPMENT TYPE AND SERVICE

Valves and reciprocating, centrifugals
stock pumps, jordans, clafflins,
hydropulpers, hydrofiners, refiners,
stock chests, white water pumps,
white liquor pumps, and black
liquor pumps.



GRAPHMAX™ PACKING

Structurally-reinforced graphite packing

APPLICATION PARAMETERS

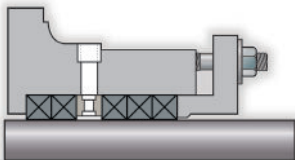
Temperature: Max. temp.
650°C (1200°F)

Chemical: pH range 0 – 14, except
oleum, fuming nitric acid, and
aqua regia

Speed: 17 m/s (3400 fpm)

EQUIPMENT TYPE AND SERVICE

Agitators, boiler feed pumps,
condensate pumps, pulpers, stock
pumps, refiners, and mixers.





329 PACKING

Stern-Lon™ flax packing

APPLICATION PARAMETERS

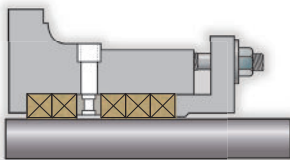
Temperature: 135°C (275°F)

Chemical: pH 6 – 8

Speed: 5 m/s (1000 fpm)

EQUIPMENT TYPE AND SERVICE

Jordans, caflins, and hydro-finers



412-W PACKING

Multi-service packing

APPLICATION PARAMETERS

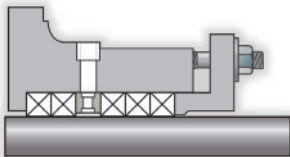
Temperature: Max. temp.
240°C (450°F)

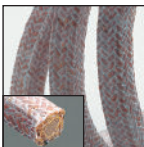
Chemical: pH range 4 – 10

Speed: 10 m/s (2000 fpm)

EQUIPMENT TYPE AND SERVICE

Mild chemicals (pH 5 – 9), cold water shafts, pocket grinder, and vacuum pumps.





1727 MULTI-LON™ PACKING

Pump packing

APPLICATION PARAMETERS

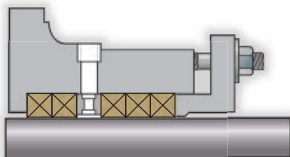
Temperature: Max. temp. 255°C (488°F) non-oxidizing

Chemical: pH range 1 – 13 unaffected by non-oxidizing acids, dilute bases, organic solvents. Should not be used in concentrated or hot sulfuric (>60%), or nitric acids (>10%), or strong bases.

Speed: 10 m/s (2000 fpm)

EQUIPMENT TYPE AND SERVICE

Mild chemicals (pH 5 – 9), centrifugals (also mech. seals), stock pumps, jordans, claffins, hydropulpers, hydrofiners, white liquor pumps, pocket grinder, and drying cylinder box.



1730 MILL PACK™ PACKING

High performance thermoset fiber packing

APPLICATION PARAMETERS

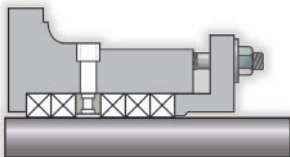
Temperature: 290°C (550°F)

Chemical: pH 1 – 13

Speed: 10 m/s (2000 fpm)

EQUIPMENT TYPE AND SERVICE

Stock agitators, stock pumps, service water, and white water.





1760 PTFE/GRAPHITE PACKING

with optional 477-1T bottom ring

Excessive heat and pressure; anti-extrusion

APPLICATION PARAMETERS

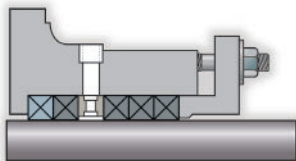
Temperature: 260°C (500°F)

Chemical: pH 0 – 14

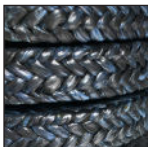
Speed: 18 m/s (3600 fpm)

EQUIPMENT TYPE AND SERVICE

Pre-steaming vessels, high and low pressure feeders, grinding stones, hydropulpers, agitators and mixers; LP/HP feeders, outlet devices, liquor pumps, and green liquor agitators.



477-1T bottom ring optional



377 CARBMAX™ PACKING

APPLICATION PARAMETERS

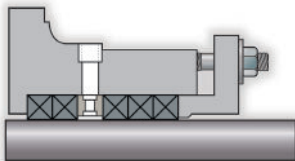
Temperature: 288°C (550°F)

Chemical: pH 1 – 14 (except strong oxidizers) *

Speed: 15 m/s (3000 fpm)

EQUIPMENT TYPE AND SERVICE

Valves and reciprocating, centrifugals, stock pumps, Jordans, claffins, hydropulpers, hydrofiners, refiners, stock chests, green liquor pumps, and lime slurry.



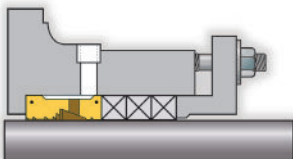
*Consult Chesterton MP Application Engineering for concerns on compatibility.



SPIRALTRAC® VERSION P ENVIRONMENTAL CONTROLLER

- Split or solid for ease of installation.
- Available in a wide variety of materials.
- No modifications required to the stuffing box.
- Replaces bottom rings of packing plus lantern ring.

EQUIPMENT TYPE AND SERVICE
Typically used in any packed application.

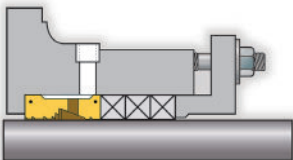


SPIRALTRAC® SUPERSET™ PACKING SET

Complete set including SpiralTrac® Version P packing set and packing rings

Applicable to all packing styles.

EQUIPMENT TYPE AND SERVICE
Black liquor, white and green liquor, TMP/CTMP refiners, thick stock pumps, hydropulpers, chemical and liquor pumps, agitators and stock pumps.



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TAMPING TOOLS

- Available in common cross sections.
- Adaptable to cut to:
 - Specific height to ensure that each ring is tamped to the bottom of the stuffing box.
 - Specific length to fit around shaft and fit into the stuffing box.

COMPRESSION PACKING INSTALLATION INSTRUCTIONS

CAUTION: Observe all depressurizing and cooling requirements, maintenance, and safety procedures before installation. Installer must follow all plant procedures and safety practices. Read all safety instructions before proceeding.

Packing Selection

Select packing and packing arrangement. Before cutting the packing rings, the correct cross-section of the packing must be determined. The shaft/sleeve diameter, stuffing box bore, and depth must be measured. The use of a vernier caliper is recommended and is the most accurate way to measure while a scale is typically used to measure the depth. Packing cross section is calculated by:

$$\text{Cross Section} = \frac{\text{Stuffing Box Diameter} - \text{Shaft/Sleeve Diameter}}{2}$$

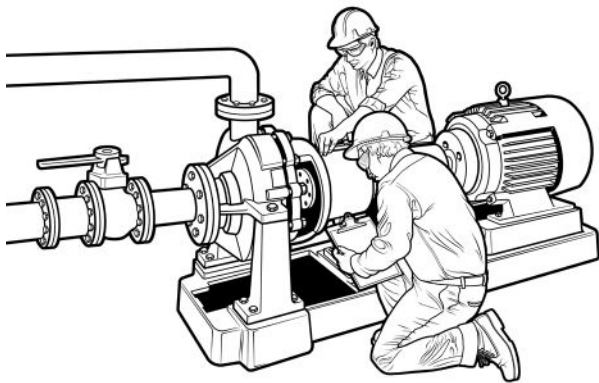
The number of rings of braided packing required is calculated by:

$$\text{Number of Rings} = \frac{\text{Stuffing Box Depth}}{\text{Cross Section}}$$

COMPRESSION PACKING INSTALLATION INSTRUCTIONS

Clean and Inspect

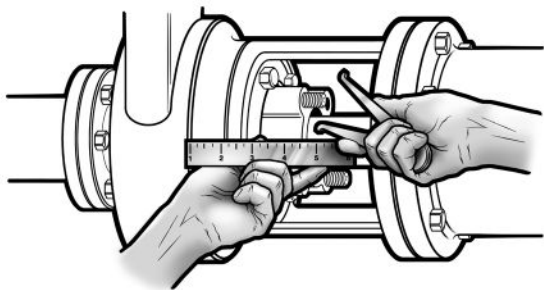
1. Unpack stuffing box using standard methods, being cautious not to nick or scratch the shaft/sleeve. Ensure that the stuffing box is completely free from used packing and any additional solids or corrosion left from the process.
2. Inspect pump shaft/sleeve to insure that it is in good condition, free from corrosion, nicks, scoring, or excessive wear. Sleeve conditions have a direct impact on the service life of packing in pumps. Replace if found defective.
3. Clean packing gland and gland follower to insure the gland can move freely into the pump stuffing box.
4. Verify that packing gland follower contacts top of stuffing box when fully inserted to insure packing will be loaded. Clean and retest if necessary.



COMPRESSION PACKING INSTALLATION INSTRUCTIONS

Measure and Document

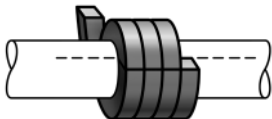
1. Measure and document the shaft/sleeve OD, stuffing box bore, and depth.
When using a lantern ring, measure from the top of the inlet port to the end of the stuffing box.



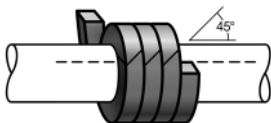
COMPRESSION PACKING INSTALLATION INSTRUCTIONS

Cut Rings

1. Wrap the packing around a mandrel of the same diameter as the pump shaft/sleeve. Mark one ring.
2. Remove from mandrel and either butt or skive cut the rings, according to detailed installation instructions for the braided packing.
3. Cut one ring at a time and check their fit on the mandrel or pump shaft/sleeve before proceeding to the equipment.



Butt cut packing

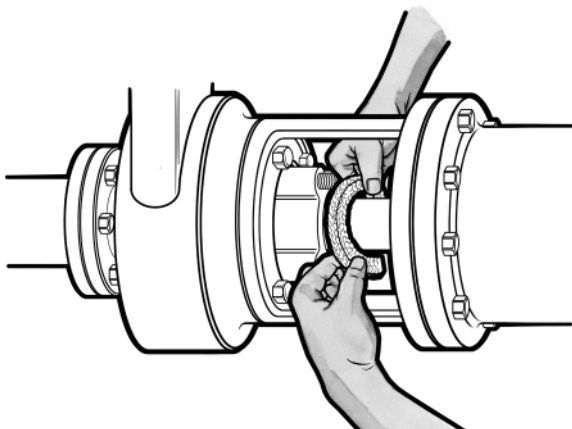


Skive cut packing

COMPRESSION PACKING INSTALLATION INSTRUCTIONS

Install

1. Install each packing ring by inserting it into the stuffing box and tamp into position with a suitable tool.
2. Ensure each ring is seated fully in the stuffing box before installing the next ring.
3. Stagger joints of subsequent rings at 90 degrees.
4. After installing the last ring, install packing gland and follower and tighten gland bolts to finger tight. Packing gland nose should slightly enter box approximately 1/8" to 3/16".
5. Start pump and tighten gland nuts.
6. Reduce leakage gradually by tightening gland nuts slowly until leakage is controlled.
7. If leakage stops completely, back off the gland and readjust to prevent packing from overheating.

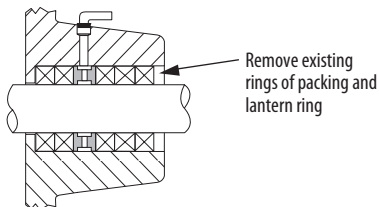


SPIRALTRAC® VERSION P ENVIRONMENTAL CONTROLLER

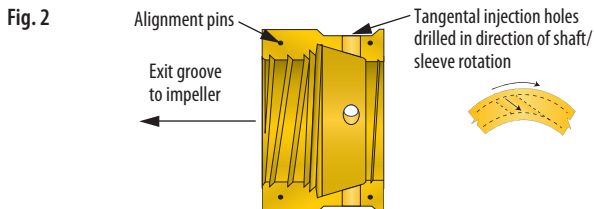
Installation Instructions

Important: In some process equipment, a flush in/flush out piping arrangement is utilized. In all cases, when using SpiralTrac Environmental Controller use flush in only and plug the flush out port. Chesterton recommends that a flowmeter and check valve be utilized on the flush line.

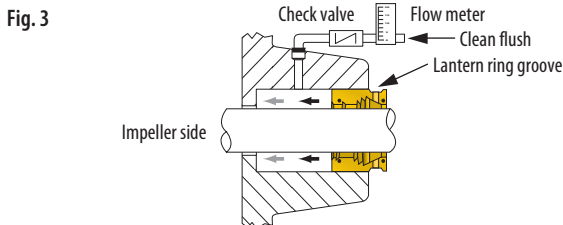
Fig. 1
Typical Stuffing Box
Arrangement



1. Disassemble Version P Type "S" split bushing. Components (Fig. 2) will be two halves of bushing with alignment pins in place.



2. Separate halves of SpiralTrac Version P and position on the shaft/sleeve as shown in Fig. 3. When installed, lantern ring groove will correspond with the injection port as shown in Fig. 4.

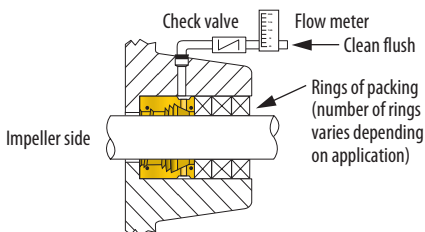


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SPIRALTRAC® VERSION P ENVIRONMENTAL CONTROLLER

Installation Instructions

Fig. 4



Note: On double ended pumps make sure the rotation is correct for each end. Rotation is determined by shaft/sleeve rotation as viewed from drive end of the pump.

3. Push the device evenly into the stuffing box.
4. Install packing rings and gland follower loosely.
5. Tighten packing to attain a drip rate leakage as per instructions of manufacturer.

Note: Self locking nut on gland studs may be required.

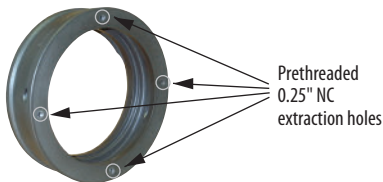
CAUTION: Do not over tighten packing.

SPIRALTRAC® VERSION P ENVIRONMENTAL CONTROLLER

Removal Instructions

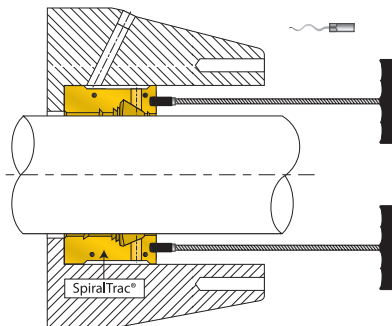
These instructions are meant as a general guide for the removal of SpiralTrac Version P devices with prethreaded extraction holes. For PTFE devices which do not have the prethreaded holes, use Option #3.

If you should encounter problems removing the SpiralTrac from the stuffing box please contact your Chesterton® representative.



Option #1

Remove worm end from two packing tools and screw the shafts/sleeves into the prethreaded 0.25" NC holes in the face of the SpiralTrac packing device and pull evenly.



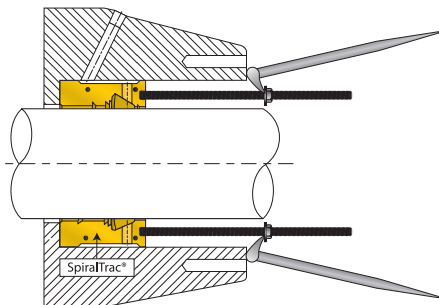
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SPIRALTRAC® VERSION P ENVIRONMENTAL CONTROLLER

Removal Instructions

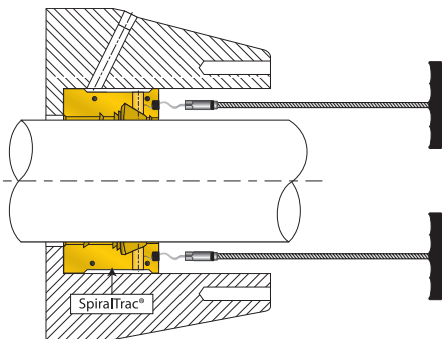
Option #2

Screw 1/4" NC (M6 x 1.0) threaded rods into the prethreaded holes in the face of the SpiralTrac® Version P. Thread nuts and washers evenly down the rods until pressure can be applied with pry bars. Then pull the SpiralTrac packing device out evenly.



Option #3—For PTFE Devices Only

Using the predrilled holes as guides, screw the worm end of the packing removal tools directly into the face of the SpiralTrac version P and pull evenly.

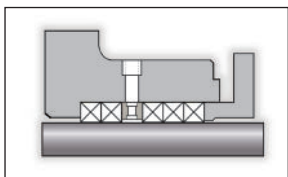


TECHNICAL REFERENCE

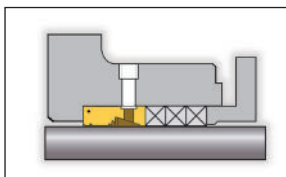
Compression Packing—Flow Rates

When flushing is required, flushwater must be connected to the lantern ring connection of the stuffing box. Flushwater supply lines should be fitted with a check valve. A flowmeter can be used to set and monitor flush rates. Flowmeters and check valves should be located as close to the stuffing box as possible. Flush pressure shall be a minimum of 15 psi or 1 bar over normal stuffing box pressure. Flow rates guidelines for flushed packing arrangements are shown as follows.

Note: SuperSet™ Packing Set flow rates shown are guidelines. In most cases flow rates can be lowered even further.



Standard 5 ring set with lantern ring



SuperSet Packing Set

Shaft Size	Standard 5 ring set with lantern ring		SuperSet™ Packing Set	
	Pumps	Agitators/ Refiners*	Pumps	Agitators/ Refiners*
inch	gpm		gpm	
<1.5	0.5		0.3	
1.5 – 2.5	0.5 – 1.0		0.3 – 0.5	
2.5 – 3.5	1.0 – 1.5	1.0 – 1.5	0.5 – 0.8	0.5 – 0.8
3.5 – 4.5	1.5 – 2.0	1.5 – 2.0	0.8 – 1.0	0.8 – 1
4.5 – 5.5	2.0 – 2.5	2.0 – 2.5	1.0 – 1.3	0.8 – 1
5.5 – 6.5	2.5 – 3.0	2.5 – 3.0	1.3 – 1.5	1.0 – 1.5
6.5 – 7.0	3.0 – 3.5	3.0 – 3.5	1.5 – 1.8	1.0 – 1.5
7.0 – 7.5	3.5 – 4.0	3.5 – 4.0	1.8 – 2.0	1.5 – 2.0
7.5 – 8.0		4.0 – 4.5		1.5 – 2.0
8.0 – 8.5		4.5 – 5.0		2.0 – 2.5

* Applicable for refiner speeds <1750 rpm

TECHNICAL REFERENCE

Compression Packing—Flow Rates

Shaft Size	Standard 5 ring set with lantern ring		SuperSet™ Packing Set	
	Pumps	Agitators/ Refiners*	Pumps	Agitators/ Refiners*
mm	l/min		l/min	
<40	2		1	
40 – 60	3 – 4		1 – 2	
60 – 80	4 – 5	4 – 5	2 – 3	2 – 3
80 – 100	5 – 6	5 – 6	3 – 4	3 – 4
100 – 120	5 – 6	5 – 6	3 – 4	3 – 4
120 – 140	6 – 7	6 – 7	4 – 5	4 – 5
140 – 160	7 – 8	7 – 8	4 – 5	4 – 5
160 – 180	8 – 10	8 – 10	5 – 6	5 – 6
180 – 200		10 – 12		6 – 7
200 – 220		12 – 14		7 – 8

* Applicable for refiner speeds <1750 rpm

Where flushing is specified, there shall be an uninterrupted source of gland sealing water that meets the following minimum criteria:

pH	: 6.5 – 8
Dissolved solids	: < 1000 ppm
Suspended solids	
>60 microns	: None
<60 microns	: <100 ppm
Hardness (Ca+, Mg+)	: <200 ppm as CaCO ₃
Temperature	: <40°C (130°F)

TECHNICAL REFERENCE

Seal Chamber Pressure Estimation

Seal chamber pressure must be known before the proper seal and flush plan can be selected. Seal chamber pressure can vary from pump design, flow rate, and fluid being pumped. Suction and discharge pressures are required to perform these calculations. Often, pump specification sheets can be old and outdated, i.e., design, operating points may have changed due to a change in process demands.

It is, for this reason, that suction and discharge pressures should be physically measured with pressure gages.

Single Stage, Single Suction, Overhung Process Pumps

Overhung centrifugal pumps are the most common process pumps in the industry. The seal chamber is located behind the pump impeller.

Seal chamber pressure can vary based on pump design. The following equations are based on closed throat design seal chambers. Pump designs include wear rings and balance holes in the impeller to reduce thrust load on the bearings. The seal chamber pressure is a function of wear ring clearance as well as size and location of the balance holes.

Quick estimate

$$P_{sb} = P_s + .25 (P_d - P_s)$$

Enclosed or semi-enclosed impellers with wear ring design and balance holes

$$P_{sb} = P_s + .05 (P_d - P_s)$$

Open impeller design with centrifugal pump-out vanes or repeller (no balance holes)

$$P_{sb} = P_s + *D (P_d - P_s)$$

**D = .3 if the impeller is at minimum diameter and .1 if the impeller is at maximum diameter.*

TECHNICAL REFERENCE

Seal Chamber Pressure Estimation

Single Stage, Double Suction Pumps

The single stage, double suction impeller is placed between bearings while the seal chambers are located adjacent to the suction eyes of the impeller. The stuffing box pressure is equal to the suction pressure.

$$P_{sb} = P_s$$

Multi-Stage Pumps

Multi-stage pumps inherently have higher discharge pressures, but low-to-medium stuffing box pressures due to impeller arrangement, casing design, balance drums and the use of balance lines. These multi-stage pumps can be mounted horizontally or vertically.

Two Stage Horizontal Pumps

Impeller arrangement can have two configurations:

1. Back to Back

In this arrangement, the seal chambers are located adjacent to the suction eye of the impeller. One chamber will see suction pressure and the other will see first stage discharge pressure.

$$P_{sb_1} = P_s$$

$$P_{sb_2} = P_s + .5 (P_d - P_s)$$

2. Eye to Eye

In this arrangement the seal chambers are located adjacent to the backside of the impeller. One chamber will see the discharge of the first stage and the other will see pump discharge pressure (second stage discharge).

$$P_{sb_1} = P_s + .5 (P_d - P_s)$$

$$P_{sb_2} = P_d$$

TECHNICAL REFERENCE

Seal Chamber Pressure Estimation

Multi-Stage Horizontal Pumps

Multi-stage boiler feed pumps are used to develop high pressures, but the seal chamber is not necessarily at a high pressure. These pumps have a low-pressure chamber (suction pressure) and a higher-pressure chamber (pressure between suction and discharge).

$$P_{sb_1} = P_s$$

Typically, a balance line is used to reduce pressure in the higher pressure seal chamber. Provided pump tolerances are in check, the higher-pressure seal chamber is as follows:

$$P_{sb_2} = P_s + 5 \text{ bar g} \\ (75 \text{ psig})$$

Note: If pump tolerances are not in check and, in the absence of a balance line, the higher-pressure chamber will be a pressure between suction and discharge pressure.

$$P_{sb_2} = P_s + 0.5 (P_d - P_s)$$

Multi-Stage Vertical Pumps

(Can or Turbine)

In these pumps the seal chamber is located at the discharge elbow. Therefore the seal chamber pressure would see discharge pressure.

$$P_{sb} = P_d$$

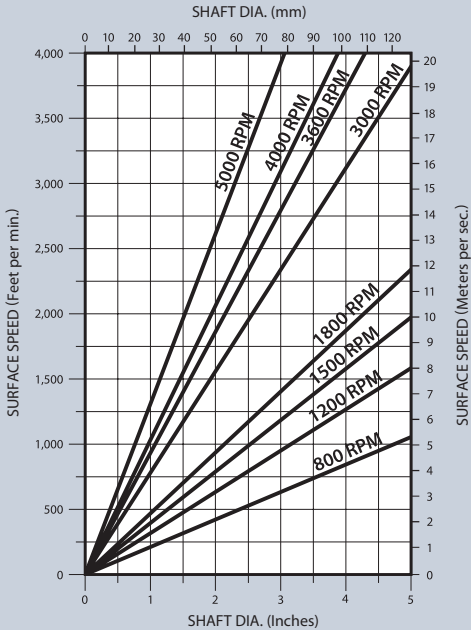
Note: The installation of a bleed-off line can reduce seal chamber pressure, provided pump tolerances are in check.

$$P_{sb_2} = P_s + 5 \text{ bar g} \\ (75 \text{ psig})$$

TECHNICAL REFERENCE

Seal Chamber Pressure Estimation

Shaft Speed Conversion Chart



Use formulas below to determine approximate shaft speeds if not shown in chart above.

$$\text{FPM} = \frac{\text{Dia. inches} \times \text{R.P.M.}}{4}$$

$$\text{M/S} = \frac{\text{Dia. millimeters} \times \text{R.P.M.}}{18750}$$

TECHNICAL REFERENCE

Seal Chamber Pressure Estimation

Metric Formulas

$$\text{Head (m)} = \frac{\text{Pressure (bar)} \times 9.8}{\text{SG}} = \frac{\text{mm Hg.} \times 0.0014}{\text{SG}}$$

$$\text{Pressure (bar)} = \frac{\text{Head (m)} \times \text{SG}}{9.8}$$

$$\text{Mm of Mercury} = \frac{\text{Head (m)} \times \text{SG}}{0.0014}$$

$$\frac{Q \text{ (l/min)} \times \text{Head (m)} \times \text{SG}}{\text{Efficiency} \times 6128}$$

Imperial Formulas

$$\text{Head (ft.)} = \frac{\text{psi} \times 2.31}{\text{sp. gr.}} = \frac{\text{In. Hg.}}{\text{sp. gr.} \times .88}$$

$$\text{BHP (centrifugal)} = \frac{\text{GPM} \times \text{head (ft.)} \times \text{sp. gr.}}{3960 \times \text{pump eff.}}$$

$$\text{PSI} = \frac{\text{head (ft.)} \times \text{sp. gr.}}{2.31} = .49 \times \text{In Hg.}$$

$$\text{BHP (Positive Disp.)} = \frac{\text{GPM} \times \text{psi}}{1715 \times \text{pump eff.}}$$

TECHNICAL REFERENCE

Units of Measure

Mariner's Measure

6 Feet = 1 Fathom

120 Fathoms = 1 Cable Length (U.S.N.)

8.439 Cable Lengths = 1 Nautical Mile

6076.12 Ft. = 1 Nautical Mile

1 Nautical Mile = 1.15 Statute Mile (International)

Inch System Conversion

Inch	X	0.0254	= Meters
Feet	X	0.305	= Meters
Yards	X	0.914	= Meters
Miles	X	1609	= Meters
Miles	X	1.609	= Kilometers
Millimeters	X	0.03937	= Inches
Centimeters	X	0.3937	= Inches
Meters	X	39.37	= Inches
Meters	X	3.281	= Feet
Meters	X	1.094	= Yards
Kilometers	X	0.621	= Miles
Sq. Centimeters	X	0.155	= Square Inches
Sq. Meters	X	10.764	= Square Feet
Sq. Meters	X	1.186	= Square Yards
Cubic Centimeters	X	0.061	= Cubic Inches
Cubic Inches	X	16.2	= Cubic Centimeters
Liters	X	0.2642	= Gallons
Gallons	X	3.78	= Liters
Cubic Meters	X	1.308	= Cubic Yards
Cubic Yards	X	0.765	= Cubic Meters

Metric System Prefixes

Mega = 1,000,000	Deci = 0.1	Tera (T) = 10^{12}
Kilo = 1,000	Centi = 0.01	Giga (G) = 10^9
Hecto = 100	Milli = 0.001	Nano (N) = 10^{-9}
Deka = 10	Micro = 0.000001	Pico (P) = 10^{-12}

TECHNICAL REFERENCE

Units of Measure

Length

1 centimeter	= 0.3937 inch	= 0.0328 foot
1 meter	= 39.37 inches	= 1.0936 yards
1 kilometer	= 0.62137 mile	= 3280 feet
1 inch	= 2.54 centimeters	
1 foot	= 0.3048 meter	
1 mil	= 0.001 inch	

Square Measure

1 sq. cm.	= 0.1550 sq. in.	
1 sq. meter	= 1.196 sq. yd.	= 10.764 sq. ft.
1 sq. kilometer	= 0.386 sq. mile	
1 sq. inch	= 6.452 sq. cm.	
1 sq. foot	= 929.03 sq. cm.	= 0.092903 sq. meter
1 sq. yard	= 0.8361 sq. meter	
1 sq. mile	= 2.59 sq. kilometers	
1 circular mil	= 0.7854 sq. mil	
1 sq. inch	= 1,000,000 sq. mils	

Cubic Measure

1 cu. centimeter = 0.061 cu. inch	1 cu. in. = 16.39 cu. cm.
1 cu. meter = 1.308 cu. yards = 35.316 cu. feet	
1 gallon (U.S.) = 231 cubic inches	
1 cu. ft. = 7.48 gallons	1 liter = 1,000 cu. centimeters

Time

1 day = 86,400 seconds	1 year = 8,760 hours (approx.)
------------------------	--------------------------------

Velocity

1 ft./sec. = 0.3048 meter/sec.	1 meter/sec. = 3.281 ft./sec.
1 ft./min. = 0.00508 meter/sec.	1 meter/sec. = 196.9 ft./min.
1 mile/hr. = 0.4470 meter/sec.	1 meter/sec. = 2.237 mi./hr.
1 kilometer/hr. = 0.2778 meter/sec.	1 meter/sec. = 3.60 km/hr.

Acceleration

1 ft./sec./sec.	= 0.3048 meter/sec./sec.
1 mile/hr./sec.	= 0.4470 meter/sec./sec.
1 kilometer/hr./sec.	= 0.2778 meter/sec./sec.
Standard gravitatio	= 9.806 meters/sec./sec.
Standard gravitatio	= 980.6 cm./sec./sec.
Standard gravitatio	= 32.2 ft./sec./sec.

TECHNICAL REFERENCE

Units of Measure

Mass

1 slug	= 32.2 pounds mass	= 14.606 kilograms
1 pound mass	= 453.6 grams	

Force

1 pound force	= 1 slug	x 1 foot sec./sec.
1 dyne	= 1 gram	x 1 centimeter/sec./sec.
1 newton	= 1 kilogram	x meter/sec./sec.
1 pound force	= 4.452 newtons	
1 newton	= 100,000 dynes	= 0.224 pound force
1 gram force	= 980.6 dynes	

Pressure

1 atmosphere	= 14.69 pounds/sq. inch	= 29.92 in. of Hg.
	= 76 cm of Hg.	= 33.9 ft. of water

1 in Hg. = 0.491 pounds/sq. inch

Water pressure pounds/sq. inch = head in ft. x 0.434

Torque

Torque is the product of force and perpendicular distance.

1 lb. - ft. = 1.356 newton-meter = 1.356 joule/radian

1 lb. - ft. = 1.356 x 10⁷ dynes-centimeter

1 lb. - ft. = 1.383 x 10⁴ grams-centimeter

1 lb. - ft. = 192 ounce-inches

Power

1 watt = 1 joule/sec.

1 horsepower = 550 ft. lb./sec. = 746 watts

1 watt = 3.413 Btu/hr = 0.239 gram calorie/sec.

P watts = R (ohms) x I (amperes)²

$$P \text{ watts} = \frac{E \text{ (volts)}^2}{R \text{ (ohms)}}$$

Angles

1 circle = 2π radians = 360 degrees

1 radian = 57.3 degrees

1 degree = 0.01745 radians

TECHNICAL REFERENCE

Units of Measure

Work and Energy – Mechanical

1 erg = 1 dyne x 1 centimeter

1 joule = 1 newton x 1 meter = 10^5 dynes x 10^2 cm = 10^7 ergs

1 ft. - lb. = 1 pound force x 1 foot = 1.356 joules

Work and Energy – Heat Equivalent

1 Btu raises 1 pound of water 1°F

1 gram calorie raises 1 gram of water 1°C

1 Btu = 252 gram calories = 778.3 ft.-lb. = 1054.8 joules

1 gram calorie = 0.003964 Btu = 4.184 joules

1 horsepower hour = 2545 Btu

Work and Energy – Electrical Equivalent

1 joule = 1 watt x 1 second = 1 amp (dc) x 1 volt (dc) x 1 sec.

W (joules) = $1/2 L$ (henries) x I^2 (amperes)²

W (joules) = $1/2 C$ (farads) x E^2 (volts)²

1 kilowatt hour = 3,600,000 joules

Geometric Figures

Circle, area of = $D^2 \times 0.7854 = \pi r^2$

r = radius

Circle, circumference of = πD or $2\pi r$

Sphere, area of = $\pi D^2 = 4\pi r^2$

D = diameter

Sphere, volume of = $D^3 \times 0.5236 = 4/3 \pi r^3$

Triangle, area of = $1/2$ altitude x base

Cone, volume of = area of base x $1/3$ altitude

Trapezoid, area of = $1/2$ (sum of parallel sides) x altitude

Pyramid, volume of = area of base x $1/3$ altitude

Miscellaneous Constants

$\pi = 3.14159$ $e = 2.71828$

$\log_e X = 2.30259 \log_{10} X$

Electronic charge = 4.5×10^{-10} e.s.u. = 1.60×10^{-20} e.m.u.

Mass units = 1.07×10^{-3} x Mev = 6.71×10^2 ergs

Speed of light = 3×10^8 meters/second

Speed of sound = (in air at sea level) = 1100 ft/second

TECHNICAL REFERENCE

Temperature Conversion Tables

NOTE_ The numbers in **BOLD FACE** refer to the temperature either in degrees Centigrade or Fahrenheit which is desired to convert into the other scale.

°C	°F	°C	°F	°C	°F	°C	°F				
-17.8	0	32.0	5.6	42	107.6	28.9	84	183.2	171	340	644
-17.2	1	33.8	6.1	43	109.4	29.4	85	185.0	177	350	662
-16.7	2	35.6	6.7	44	111.2	30.0	86	186.8	182	360	680
-16.1	3	37.4	7.2	45	113.0	30.6	87	188.6	188	370	698
-15.6	4	39.2	7.8	46	114.8	31.1	88	190.4	193	380	716
-15.0	5	41.0	8.3	47	116.6	31.7	89	192.2	199	390	734
-14.4	6	42.8	8.9	48	118.4	32.2	90	194.0	204	400	752
-13.9	7	44.6	9.4	49	120.2	32.8	91	195.8	210	410	770
-13.3	8	46.4	10.0	50	122.0	33.3	92	197.6	216	420	788
-12.8	9	48.2	10.6	51	123.8	33.9	93	199.4	221	430	806
-12.2	10	50.0	11.1	52	125.6	34.4	94	201.2	227	440	824
-11.7	11	51.8	11.7	53	127.4	35.0	95	203.0	232	450	842
-11.1	12	53.6	12.2	54	129.2	35.6	96	204.8	238	460	860
-10.6	13	55.4	12.8	55	131.0	36.1	97	206.6	243	470	878
-10.0	14	57.2	13.3	56	132.8	36.7	98	208.4	249	480	896
-9.4	15	59.0	13.9	57	134.6	37.2	99	210.2	254	480	914
-8.9	16	60.8	14.4	58	136.4	37.8	100	212.0	260	500	932
-8.3	17	62.6	15.0	59	138.2				266	510	950
-7.8	18	64.4	15.6	60	140.0	43.3	110	230	271	520	968
-7.2	19	66.2	16.1	61	141.8	48.9	120	248	277	530	986
-6.7	20	68.0	16.7	62	143.6	54.4	130	266	282	540	1004
-6.1	21	69.8	17.2	63	145.4	60.0	140	284	288	550	1022
-5.6	22	71.6	17.8	64	147.2	65.6	150	302	293	560	1040
-5.0	23	73.4	18.3	65	149.0	71.1	160	320	299	570	1058
-4.4	24	75.2	18.9	66	150.8	76.7	170	338	304	580	1076
-3.9	25	77.0	19.4	67	152.6	82.2	180	356	310	590	1094
-3.3	26	78.8	20.0	68	154.4	87.8	190	374	316	600	1112
-2.8	27	80.6	20.6	69	156.2	93.3	200	392	321	610	1130
-2.2	28	82.4	21.1	70	158.0	98.9	210	410	327	620	1148
-1.7	29	84.2	21.7	71	159.8	100	212	413	332	630	1166
-1.1	30	86.0	22.2	72	161.6	104	220	428	338	640	1184
-.6	31	87.8	22.8	73	163.4	110	230	446	343	650	1202
0	32	89.6	23.3	74	165.2	116	240	464	349	660	1220
.6	33	91.4	23.9	75	167.0	121	250	482	354	670	1238
1.1	34	93.2	24.4	76	168.8	127	260	500	360	680	1256
1.7	35	95.0	25.0	77	170.6	132	270	518	366	690	1274
2.2	36	96.8	25.6	78	172.4	138	280	536	371	700	1292
2.8	37	98.6	26.1	79	174.2	143	290	554	377	710	1310
3.3	38	100.4	26.7	80	176.0	149	300	572	382	720	1328
3.9	39	102.2	27.2	81	177.8	154	310	590	388	730	1346
4.4	40	104.0	27.8	82	179.6	160	320	608	393	740	1364
5.0	41	105.8	28.3	83	181.4	166	330	626	399	750	1382

TECHNICAL REFERENCE

Temperature Conversion Tables

NOTE_ The numbers in **BOLD FACE** refer to the temperature either in degrees Centigrade or Fahrenheit which is desired to convert into the other scale.

°C		°F	°C		°F	°C		°F
404	760	1400	638	1180	2156	871	1600	2912
410	770	1418	643	1190	2174	877	1610	2930
416	780	1436	649	1200	2192	882	1620	2948
421	790	1454	654	1210	2210	888	1630	2966
427	800	1472	660	1220	2228	893	1640	2984
432	810	1490	666	1230	2246	899	1650	3002
438	820	1508	671	1240	2264	904	1660	3020
443	830	1526	677	1250	2282	910	1670	3038
449	840	1544	682	1260	2300	916	1680	3056
454	850	1562	688	1270	2318	921	1690	3074
460	860	1580	692	1280	2336	927	1700	3092
466	870	1598	699	1290	2354	932	1710	3110
471	880	1616	704	1300	2372	938	1720	3128
477	890	1634	710	1310	2390	943	1730	3146
482	900	1652	716	1320	2408	949	1740	3164
488	910	1670	721	1330	2426	954	1750	3182
493	920	1686	727	1340	2444	960	1760	3200
499	930	1706	732	1350	2462	966	1770	3218
504	940	1724	738	1360	2480	971	1780	3236
510	950	1742	743	1370	2498	977	1790	3254
516	960	1760	749	1380	2516	982	1800	3272
521	970	1778	754	1390	2534	988	1810	3290
527	980	1796	760	1400	2552	993	1820	3308
532	990	1814	765	1410	2570	999	1830	3326
538	1000	1832	771	1420	2588	1004	1840	3344
543	1010	1850	777	1430	2606	1010	1850	3362
549	1020	1868	782	1440	2624	1016	1860	3380
554	1030	1886	788	1450	2642	1021	1870	3398
560	1040	1904	793	1460	2660	1027	1880	3416
566	1050	1922	799	1470	2678	1032	1890	3434
571	1060	1940	804	1480	2696	1038	1900	3452
577	1070	1958	810	1490	2714	1043	1910	3470
582	1080	1976	816	1500	2732	1049	1920	3488
588	1090	1994	821	1510	2750	1054	1930	3506
593	1100	2012	827	1520	2768	1060	1940	3524
599	1110	2030	832	1530	2786	1066	1950	3542
604	1120	2048	838	1540	2804	1071	1960	3560
610	1130	2066	843	1550	2822	1077	1970	3578
616	1140	2084	849	1560	2840	1062	1980	3596
621	1150	2102	854	1570	2856	1088	1990	3614
627	1160	2120	860	1580	2876	1093	2000	3632
632	1170	2138	866	1590	2894			

TECHNICAL REFERENCE

Other Handy Formulas

Power Transmission by Shaft

$$HP = [\text{Torque (in lb - ft)} \times \text{rpm}] \div 5250$$

Power to Drive Pump

$$HP = \frac{\text{Gal. per min.} \times \text{total head (inc. friction)}}{3,960 \times \text{eff. of pump}}$$

Where: Approx. friction head (ft.) =

$$\frac{\text{pipe length (ft.)} \times [\text{velocity of flow (fps)}]^2 \times 0.02}{5.367 \times \text{diameter (in.)}}$$

Eff. = Approximately 0.50 to 0.85

Formula for Problems Involving Rotating Masses

Time required to change speed of rotating mass from N_1 to N_2 rpm.

$$t = \frac{(Wr^2) (N_2 - N_1)}{(308) (\text{torque lb - ft})} \text{ Sec.}$$

Where (Wr^2) = Flywheel effect.

Kinetic energy of rotating mass.

$$K.E. = \frac{(WK^2) (\text{rpm}^2)}{5870} \quad \text{ft - lbs} = \frac{(WK^2) (\text{rpm}^2)}{3.23 \times 10^6} \text{ hp. sec.}$$

Where W = Weight (lbs.)

K = Radius of gyration (ft.)

Induction Motor Acceleration Loss.

$$\text{Loss} \cong \left(1 + \frac{R_1}{R_2}\right) \frac{WK^2 (N_2 - N_1)^2}{3.23 \times 10^6} \text{ hp. sec.}$$

Where R_1 and r_2 = stator and rotor resistances.

Stored energy constant.

$$H = \frac{0.231 (Wr^2) (\text{rpm})^2 10^{-6}}{\text{kva}} \text{ kw. sec. per kva.}$$

Transfer of WK_2 Through a Gear.

$$W \frac{2}{1} = W \frac{2}{2} \left(\frac{N_2}{N_1}\right)^2$$

TECHNICAL REFERENCE

Common Fractions Reduced to Decimals

8ths	16ths	32nds	64ths	Decimal
			1	.015625
		1	2	.03125
			3	.046875
	1	2	4	.0625
			5	.078125
		3	6	.09375
			7	.109375
1	2	4	8	.125
			9	.140625
		5	10	.15625
			11	.171875
	3	6	12	.1875
			13	.203125
		7	14	.21875
			15	.234375
2	4	8	16	.25
			17	.265625
		9	18	.28125
			19	.296875
	5	10	20	.3125
			21	.328125
		11	22	.34375
			23	.359375
3	6	12	24	.375
			25	.390625
		13	26	.40625
			27	.421875
	7	14	28	.4375
			29	.453125
		15	30	.46875
			31	.484375
4	8	16	32	.5

8ths	16ths	32nds	64ths	Decimal
			33	.515625
		17	34	.53125
			35	.546875
	9	18	36	.5625
			37	.578125
		19	38	.59375
			39	.609375
5	10	20	40	.625
			41	.640625
		21	42	.65625
			43	.671875
	11	22	44	.6875
			45	.703125
		23	46	.71875
			47	.734375
6	12	24	48	.75
			49	.765625
		25	50	.78125
			51	.796875
	13	26	52	.8125
			53	.828125
		27	54	.84375
			55	.859385
7	14	28	56	.875
			57	.890625
		29	58	.90625
			59	.921875
	15	30	60	.9375
			61	.953125
		31	62	.96875
			63	.934375
8	16	32	64	1.00000

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